

# Environmental benefits and economic feasibility of a photovoltaic assisted heat pump water heater

F. Aguilar<sup>a</sup>, D. Crespi-Llorens<sup>a</sup>, P.V. Quiles<sup>a</sup>

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<sup>a</sup>Dep. Ing. Mecánica y Energía. Universidad Miguel Hernández de Elche. Av. de la Universidad s/n (03202). Elche (Spain).

## Abstract

This work presents a techno-economic study which evaluates the environmental benefits and the economic feasibility of a photovoltaic assisted compact heat pump water heater. The system heats water for domestic consumption in a 190 litres tank. The heat pump is simultaneously powered by the grid and PV panels, although the system was designed to prioritize the PV energy supply. The system does not use batteries and does not feed electricity to the grid.

Based on experimental measurements during one year, the study analyses the efficiency of the system for a 4 family members domestic hot water (DHW) consumption. The experimental data shows that the system is friendly to the grid, showing low peak loads and not feeding to the grid.

A techno-economic analysis which considers the lifetime cost of the system as well as its environmental benefits has been carried out. The techno-economic analysis shows the benefits of this system when it is compared to: a DHW heat pump without PV, an electrical heater, a boiler and a boiler + solar thermal collectors. The total annualized cost of the system, for a period of 25 years and an electricity price of 0.2 €/kWh, has been quantified at 337 €/year. Furthermore, the system has been found to reduce the non-renewable primary energy consumption by 79% and the CO<sub>2</sub> emissions by 82% in comparison with a boiler.

Finally, experimental correlations of the system performance are proposed, so that the results of this work can be extended to other locations with similar climates.

**Keywords:** photovoltaics, solar energy, heat pump, water heater, economic feasibility, environmental impact

1	<b>Nomenclature</b>	12	$FSAV$	Fraction savings.	
2	$E_{HP}$	Electricity consumption by the heat pump.	13	$I$	Solar irradiation.
3	$E_{PV}$	Photovoltaic production.	14	$P$	Power.
4	$E_{PV,HP}$	Part of the photovoltaic production which is consumed by the heat pump.	15	$nRPE$	Non-renewable primary energy.
5			16	$PEF$	Primary energy factor.
6	$E_{PV,RES}$	Part of the photovoltaic production which is consumed by the resistance inside the DHW tank to directly heat the DHW.	17	$PER_{nRE}$	Primary energy ratio defined as the nRPE consumed by a system over the nRPE consumed by the reference system.
7			18		
8			19		
9	$E_{GD}$	Electricity consumption from the grid (by the heat pump).	20	$Q_{TOT}$	Total thermal energy provided by the system to the water inside the tank.
10			21		
11	$\bar{\eta}$	Average seasonal efficiency.	22	$Q_{DHW}$	Useful thermal energy for domestic hot water production.
			23		

Email address: dcrespi@umh.es (D. Crespi-Llorens)

24	$Q_L$	Water tank thermal losses.
25	$Q_{HP}$	Thermal energy produced by the heat pump.
26	$Q_{RES}$	Thermal energy produced by Joule effect at
27		the electrical resistance.
28	$SC$	Solar contribution.
29	$SPF$	Seasonal performance factor. It is the ef-
30		iciency of a device or system, calculated
31		as the ratio of the heat provided by the
32		device/system and its total electric energy
33		consumption over a period of time.
34	<u>Subindices</u>	
35	<i>boiler</i>	Boiler system.
36	$CO_2$	Refers to $CO_2$ emissions.
37	$EL$	Electricity.
38	$GD$	Electrical grid.
39	$HP$	Heat pump.
40	$HP + PV$	Heat pump powered by photovoltaic panels
41		and the grid.
42	$NG$	Natural Gas.
43	$nRPE$	Non-renewable primary energy.
44	$PV$	Photovoltaic panels.
45	$RES$	Resistance.
46	<i>ref</i>	Reference system.
47	$TH$	Thermal energy.

## 48 1. Introduction

49 The Paris Agreement's central aim is to strengthen  
50 the global response to the threat of climate change by  
51 keeping a global temperature rise this century well be-  
52 low  $2^\circ\text{C}$  above pre-industrial levels and to pursue efforts  
53 to limit the temperature increase even further to  $1.5^\circ\text{C}$ ".

54 The EU efforts in relation to progress towards the  
55 goal set in the Paris Agreement are clearly established  
56 for the building sector in recently approved Direc-  
57 tives (2018/2001/EU; 2018/844/EU). The pathway to-  
58 wards the objective of decarbonized buildings by the  
59 year 2050 is established in the 2018/844/EU. It implies  
60 that current fossil fuel equipment (boilers) for DHW  
61 production will be replaced by environmental friendly

62 solutions, probably involving heat pumps. In addition,  
63 the EU has set a binding target to reduce emissions by  
64 at least 40% below 1990 levels by 2030.

65 The promotion of the use of energy from renewable  
66 sources like heat pumps, geothermal, solar photovoltaic  
67 and solar thermal systems will be one of the key ways  
68 to achieve these challenges (2018/2001/EU). Last but  
69 not least, Directive 2018/2001/EU states that Member  
70 States should try to minimize the overall cost of decar-  
71 bonized systems.

72 In this framework, the application of efficient heat  
73 pumps with the possible support of solar thermal or pho-  
74 tovoltaic energy is presented as a solution to be con-  
75 sidered in future nearly zero energy buildings. In res-  
76 idential buildings, from the design point of view, the  
77 DHW demand cannot be reduced and the hot water can  
78 be accumulated (water tanks). Therefore, solar-assisted  
79 compression heat pumps SACHP for the production of  
80 domestic hot water are very suitable systems to operate  
81 depending on the availability of solar thermal or pho-  
82 tovoltaic energy.

83 Much research on SACHP water heaters has been car-  
84 ried out during the last 20 years. Most of it is focused on  
85 solar thermal energy use in the evaporator of the com-  
86 pression heat pumps. Two types are considered: direct  
87 expansion solar heat pumps (DX-SAHP) when refrig-  
88 erant flows through the solar collector or indirect ex-  
89 pansion solar heat pumps (IDX-SAHP) when there is a  
90 heat exchanger between the refrigerant and the fluid that  
91 flows through the solar collector. Many of these works  
92 are presented in Wang et al. (2017) and Mohanraj et al.  
93 (2018) reviews, where it is found that air heat pumps  
94 in the application of domestic hot water at present have  
95 typical SPF (seasonal COP) between 2.5 and 3.5 when  
96 water preparation temperature is below  $50^\circ\text{C}$ , and this  
97 performance can be improved to 6-9 by adding a solar  
98 contribution to the system.

99 In recent years, photovoltaic solar energy has also  
100 been considered in the behavior of SAHP. The recently  
101 published review of Mohanraj et al. (2018) includes a  
102 section about "Solar photovoltaic assisted heat pump  
103 water heaters". Some works like Chow et al. (2010) and  
104 Fang et al. (2010) are focused on DX-SACHP with PVT  
105 evaporators that improve at the same time the COP of  
106 the heat pump and the efficiency of the PV panels. Any-  
107 way, in a real application it should be considered that  
108 when the SACHP is stopped, PVT efficiency is usually  
109 lower than standard PV. In these works, photovoltaic  
110 electricity is exported and not considered to be a part  
111 of the system.

112 Indirect expansion solar heat pumps IDX-SACHP  
113 with PVT have also been studied. Wang et al. (2015) in-

114 investigated the efficiency of an IDX-SACHP with a PVT 166  
115 of water recirculation. The installation accumulates the 167  
116 water heated by the PVT, being able to combine better 168  
117 with the heat pump through a water/coolant exchanger. 169  
118 To overcome the difficulties remaining in the existing 170  
119 PVT technologies, Zhang et al. (2013) and Li and Sun 171  
120 (2018) propose to use heat pipes as part of the PVT 172  
121 panels. They obtained an overall coefficient of system per- 173  
122 formance much higher than traditional heat pump sys- 174  
123 tems and the photovoltaic efficiency was also improved. 175

124 A different approach to the efficiency of the system 176  
125 should be carried out when photovoltaic energy cannot 177  
126 be exported or when the benefits of this excess elec- 178  
127 tricity are not obtained. The last revision of the Euro- 179  
128 pean EPBD directive established a new *Smart Readiness* 180  
129 *Indicator* as a parameter to measure the capacity 181  
130 of buildings to adapt their operation to the needs of the 182  
131 occupants and the grid and to improve the energy effi- 183  
132 ciency and overall performance of buildings. In this 184  
133 research line, Kato and Suzuoki (2014) carried out sim- 185  
134 ulations to demonstrate that it is possible to use heat 186  
135 pump water heaters (HPWH) in homes to improve the 187  
136 operation of the electricity network in residential areas 188  
137 with many photovoltaic installations. Their proposal 189  
138 was an autonomous scheduling of HPWH so that the 190  
139 aggregated electricity consumption by a number of HP- 191  
140 WHs follows the daily change in power supply of the 192  
141 photovoltaic system. Their study focused on the elec- 193  
142 trical analysis of the system, making an energy balance, 194  
143 but without considering the possible requirements of the 195  
144 DHW demand (possible problems of low temperature 196  
145 and discomfort). Sichilalu and Xia (2015) developed a 197  
146 scheduling model for heat pump water heater (HPWH) 198  
147 in order to optimize the energy control of a grid-tied 199  
148 photovoltaic. They assess that the collective effort re- 200  
149 quired to turn a new or existing building into a NZEB 201  
150 involves proper selection of an appropriate technology, 202  
151 application of optimal control in energy demand. Poulet 203  
152 and Outbib (2015) analysed hybrid systems using re- 204  
153 newable energy sources without any connection to an 205  
154 electrical network. After their experience, they came to 206  
155 the conclusion that the optimal design consisted of pho- 207  
156 tovoltaic panels + air/water heat pumps with improved 208  
157 control which includes strategies based on the weather 209  
158 forecast. 210

159 Thygesen and Karlsson (2014) studied the perfor- 211  
160 mance of PV solar assisted heat pump water heaters 212  
161 with two different storage systems: a battery and a hot 213  
162 water tank. They concluded that thermal storage and 214  
163 eventually a PV controlled heat pump is the most cost 215  
164 effective system, since the objective should be to reduce 216  
165 the purchase of electricity. 217

The approach of the authors (Aguilar et al., 2016) fo-  
cused on improving the performance of a photovoltaic  
assisted heat pump for domestic water heating appli-  
cations. The photovoltaic panels are connected di-  
rectly to the unit and the photovoltaic electricity is only  
consumed in the system: either in the compressor or  
in the electric heater. The heat pump analysed is an  
ON/OFF unit with a nominal heating capacity of 1.5 kW  
and a nominal electrical consumption of 470 W (nomi-  
nal COP=3.19). The system has a thermal storage of  
190 litres and no batteries.

Mohanraj et al. (2018) pointed out that in solar as-  
sisted compression heat pumps (SACHP), further re-  
search is needed on some specific topics like *Techno*  
*economical feasibility evaluation of SACHP systems for*  
*different applications.*

Poppi et al. (2018) reviewed techno-economic stud-  
ies of hybrid renewable energy systems that combine ST  
(solar thermal) and/or PV with heat pumps for residen-  
tial heating applications (space heating and DHW pro-  
duction). In their study, the payback was shown to be  
dependent on solar irradiance and heating degree-days.  
Moreover, they pointed out that the inclusion of PV into  
heat pump systems further complicates the analysis in  
order to clearly define where the system boundary must  
be for a transparent energetic and economic assessment  
of solar assisted heat pumps. In fact, they proposed the  
“building boundary level” to better understand energetic  
and economic potential of PV heat pump systems (the  
surplus PV energy was not considered).

Payback of PV and heat pump systems can vary  
significantly according to metering policies in place  
(Thygesen and Karlsson, 2013). They analyzed 3 solar  
assisted ground source heat pump systems and con-  
cluded that the conjunction with a PV-system is the most  
effective system with regards to energy and economics.

Li and Sun (2018) found that compared with a tra-  
ditional heat pump water heater, although extra \$368.2  
should be paid for the initial cost of the PVT system,  
about 29.6% of life cycle cost could be saved.

In this context, this work presents a detailed technical  
and economic study of the system that was experimen-  
tally measured by the authors in Aguilar et al. (2016).  
Correlations of the system performance are provided so  
that the results can be extended to other locations. The  
boundary for the energetic and economic assessment is  
considered to be the system itself, since all the PV en-  
ergy is consumed in the water heater. An economic  
analysis which considers the lifetime cost of the system  
has been carried out. The proposed system is  
compared to other 5 widely spread water heater systems  
in terms of primary energy consumption and economic

Table 1: Technical data of the compact heat pump and the photovoltaic panels.

(a) Compact heat pump model: MIDEA Compak KHP 15 190.

Parameter	Value	Units
Heating capacity	1500	W
Compressor electrical power	470	W
Coefficient of performance (*)	3.19	-
Electrical heater power	2000	W
Refrigerant	R134a	-
Evaporator fan power	30	W
Tank volume	190	L

(\*) Manufacturer test conditions: Input/output water of 15°C / 55°C. Outside wet/dry bulb of 15°C / 20°C.

(b) Technical data of the photovoltaic panels.

Parameter	Value	Units
Nominal power	235	Wp
Efficiency	13.74	%

savings. In addition, the interaction of the system with the network, its peak loads and its adjustment with the photovoltaic production have also been analysed.

## 2. Experimental setup

The system under study (*HP+PV*), depicted in Figure 1, consists of a compact heat pump connected simultaneously to two PV panels of 235 Wp each (see Table 1) and to the electrical grid. An MPPT micro-inverter connected to the PV panels converts direct current (24-30 VDC) to alternating (230 VAC).

The coupling between the heat pump, the photovoltaic panels and the electrical network is carried out by means of a network current inhibitor. This device prioritizes the PV energy supply over the one from the grid, in order to maximize the use of solar energy. Consequently, if PV production is sufficient to power the heat pump, no grid electricity is consumed. Electricity consumption from the grid is only required when the PV panels' production is not enough to completely feed the heat pump. In this case, the grid will provide the difference between the panels' production and the heat pump consumption. When the heat pump is OFF and the PV panels produce electricity, this energy is consumed by an electrical resistance inside the water tank. In any case, the total energy produced by the PV panels is used by the system for DHW production (by the heat pump or by the electrical resistance). The objective of

this configuration is to minimize electricity consumption from the grid.

Figure 1 also shows the energy flows (thermal and electrical) within the HP+PV system. From them, the equations describing the system may be defined. Equation 1 describes that the electricity produced by the PV panels can be used to power the heat pump and/or to feed the electrical resistance inside the water tank.

$$E_{PV} = E_{PV,HP} + E_{PV,RES} \quad (1)$$

Besides, the heat pump can be powered with electricity from the PV panels and/or from the grid.

$$E_{HP} = E_{PV,HP} + E_{GD} \quad (2)$$

The thermal energy  $Q_{TOT}$  is provided to the water by the heat pump  $Q_{HP}$  and the electrical resistance  $Q_{RES}$ , and it is used for DHW production  $Q_{DHW}$  and to compensate for energy losses  $Q_L$ .

$$Q_{TOT} = Q_{HP} + Q_{RES} \quad (3)$$

$$Q_{TOT} = Q_{DHW} + Q_L \quad (4)$$

Furthermore, the following indicators, which evaluate the performance of the system, have been defined. On the one hand, the seasonal performance factor of the heat pump is defined as the coefficient between the thermal energy provided by the heat pump and its electrical consumption in real working conditions throughout a year.

$$SPF_{HP} = \frac{Q_{HP}}{E_{HP}} \quad (5)$$

On the other hand, the solar contribution has been defined as the ratio between the heat produced by the heat pump or the electrical resistance using electricity from the PV panels and the total heat produced.

$$SC = \frac{Q_{PV}}{Q_{TOT}} = \frac{Q_{RES} + Q_{HP} (E_{PV,HP}/E_{HP})}{Q_{RES} + Q_{HP}} \quad (6)$$

A deeper analysis of the HP+PV system in relation with the aforementioned performance indicators was presented in a previous work by the authors (Aguilar et al., 2016).

The use of energy of the system can be better observed in Figure 2, where one day results are shown. The light grey area corresponds to energy produced by the PV panels which is consumed by the heat pump  $E_{PV,HP}$ . The area in dark grey belongs to energy from the electrical grid which is consumed by the heat pump

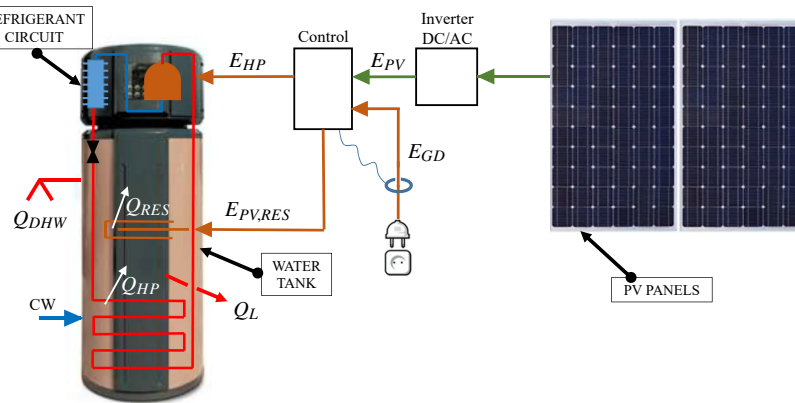


Figure 1: Sketch of photovoltaic assisted heat pump for domestic hot water production (HP+PV system).

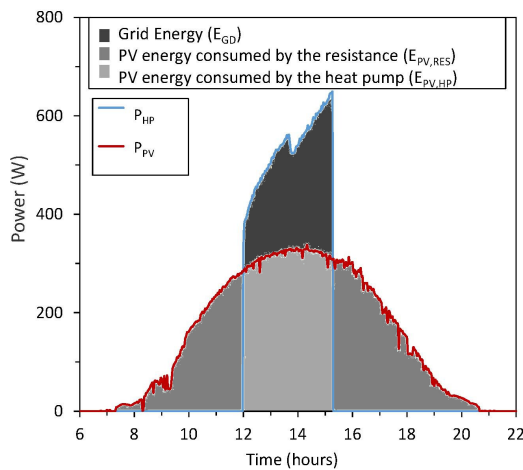


Figure 2: Energy flows within the experimental setup during one day of operation.

$E_{GD}$ . Lastly, middle grey has been used to color the energy produced by the PV panels which is consumed by the electrical resistance inside the DHW tank  $E_{PV,RES}$ , directly used to heat water ( $Q_{RES} = E_{PV,RES}$ ).

### 2.1. Experimental facility

In order to test the described system during one year, an experimental facility was built on the roof of the university research laboratory, located in Elche (Southeast of Spain).

Figure 3 shows the facility, where subsystems A (heat pump and DHW tank) and B (power sources) have already been described. In subsystem B, the solar panels are facing South with an inclination of  $45^\circ$ . In order to emulate domestic hot water consumption without wasting water, subsystem C has been used. It has an auxiliary tank which receives hot water at  $55\text{--}60^\circ\text{C}$  from the

heat pump and a water chiller which cools it down to  $12\text{--}15^\circ\text{C}$ .

Besides, several probes and measuring instruments have been installed along the facility in order to measure: meteorological data, refrigerant cycle temperatures and pressures, water flowrate and power consumption (from the grid and from the PV panels). All the instruments and probes are connected to an HP 34970A data acquisition unit, which makes recordings every minute.

The facility has been used to emulate the consumption of a 4 member family. For this number of people, a daily consumption of 132 litres at  $55^\circ\text{C}$  has been estimated in agreement with the Spanish regulation (CTE DB-HE4) and the standard UNE-EN 16147. In an effort to imitate the consumption in a real dwelling, where hot water is consumed throughout the morning, the afternoon and the evening, 6 water tapings of 22 litres each have been programmed every day. Each one has been carried out at 4 L/min with a duration of 5.5 minutes at the following local times 7:30, 8:15, 10:00, 13:45, 21:00, 22:00.

The heat pump has been configured to start operation at 10:00 a.m. (solar time) and stop when the DHW preparation temperature of  $55^\circ\text{C}$  has been reached.

Electrical measurements uncertainties on voltage and current are lower than 1% for 95% of confidence level. They yield to a power measurement uncertainty of less than 1.5% and an uncertainty lower than 2% in the calculated solar contribution,  $SC$ , (JCGM 100:2008).

Further details of the experimental setup have been provided in a previous work (Aguilar et al., 2016).

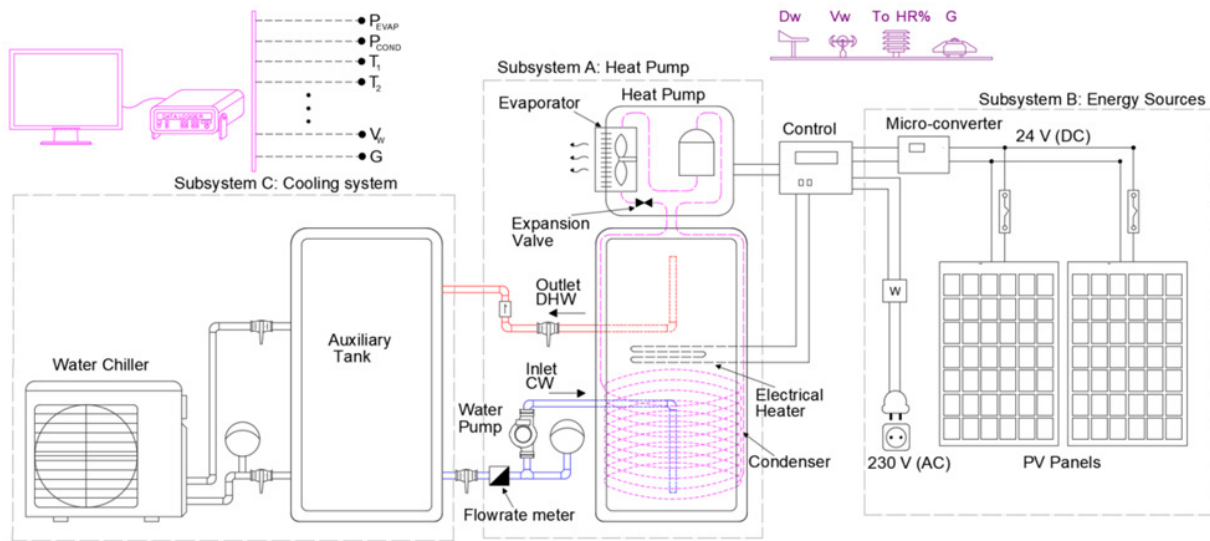


Figure 3: Experimental facility.

### 3. Results

As has been mentioned before, the aim of this work is to verify and highlight the benefits of the system under study for domestic hot water (DHW) production. Such benefits can be summarised as:

1. The use of electricity as a better energy source than the direct use of fossil fuels (decarbonization).
2. The reduced impact of the system on the electrical grid (grid friendly system).
3. The reduction in primary energy consumption as well as CO<sub>2</sub> emissions.
4. The reduced annualized cost of the system.

The following subsections analyse each of the former points. Additionally, the tools to extend the results of this section to different regions around the world with Mediterranean climate conditions have been included in Section 3.5.

#### 3.1. Decarbonization

The first argument has been pointed out by the European Union as an effective way of reducing CO<sub>2</sub> emissions, together with a higher percentage of renewable energy production in the grid. In fact, the European Union has set the goal of full decarbonization of buildings before 2050. It can be stated that heat pumps for domestic hot water production will play a key role in achieving this.

The consumption of hot water in homes can be increased by adding the water consumption of household appliances: washing machine and dishwasher.

In future nZEB homes, where heating and cooling demand will be reduced, the optimization of the DHW production system will be very important to reach the goal of decarbonisation. The design of the heat pumps must be carried out in such a way that they should work taking into account the available renewable energy: usually photovoltaic solar energy. The heat pump can operate in sunny hours and store the thermal energy in the tank: hence the importance of the design and dimensioning of the system.

In this sense, this study shows the results of a year of operation of a compact heat pump of 1.5 kW (thermal) with a tank of 190 liters, operating for a typical DHW consumption of a family of 4 members. The system only consumed 317.6 kWh of electricity from the grid in one year (cost of about 50 €/year).

#### 3.2. Impact of the system on the grid

In order to evaluate the impact of the system on the grid, Figure 4 has been plotted. It shows the heat pump electricity consumption, the PV panels' production and how much electricity is consumed from the grid. This data is plotted throughout one week for three different periods of the year: January, April and June.

As can be observed, the starting time of the heat pump (10:00 a.m., solar time) has been selected in order to maximize the use of PV electricity. The results also show that the electricity consumption peak could reach a maximum of about 600 W, on the rare occasions when there is no PV production at all. Furthermore, if there is good photovoltaic generation, the max-

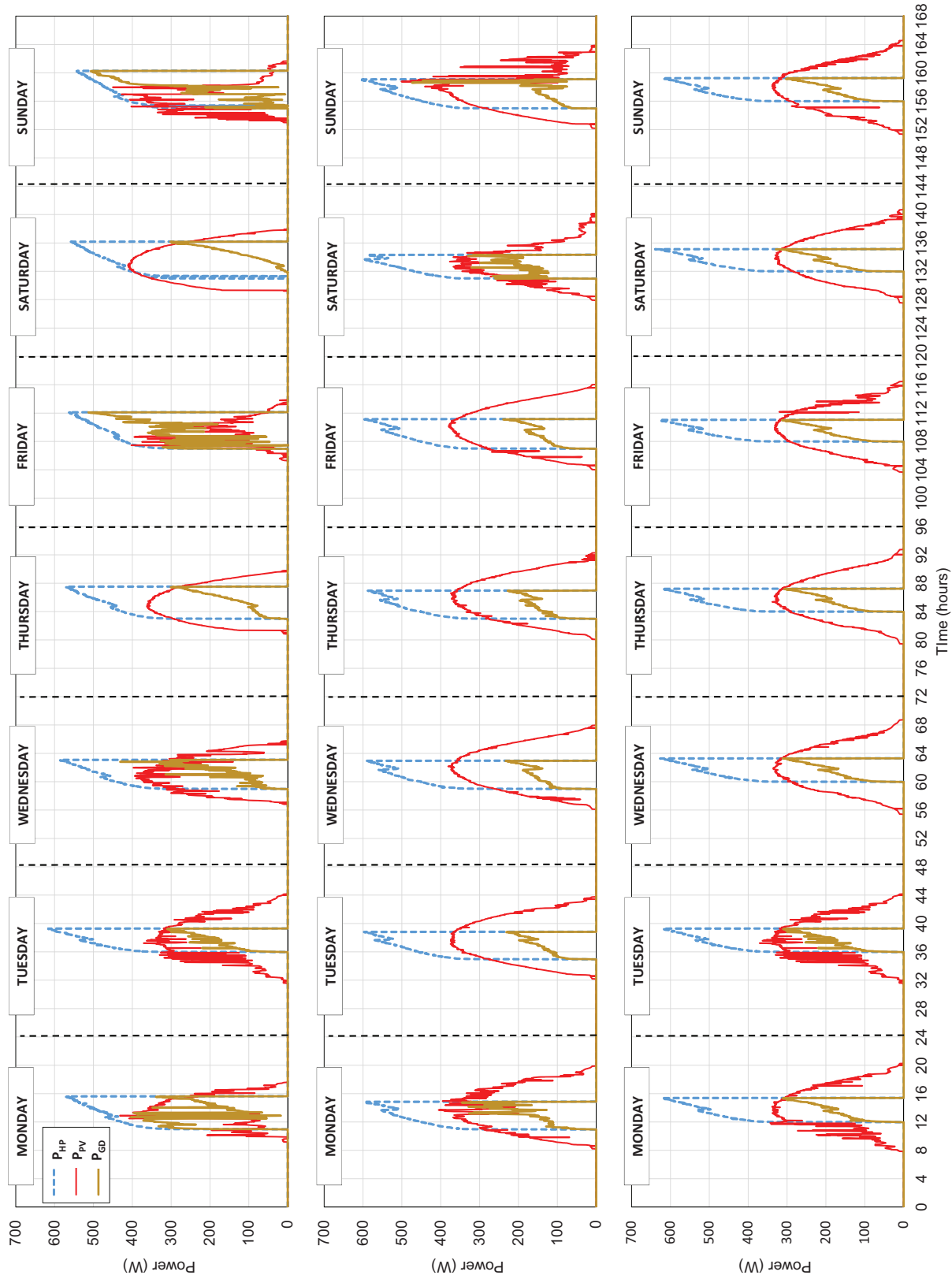


Figure 4: Electricity production and consumption during one week of January (top), April (middle) and June (bottom).

imum grid electricity consumption is about 300 W. In any case, consumption peaks are very low by using this system, which is a significant advantage in comparison for example with an electric heater. Moreover, the photovoltaic electricity surplus does not feed the grid but a resistance inside the DHW tank (Figure 2), and thus unplanned and potentially problematic electricity supply from the PV panels to the grid is avoided.

### 3.3. Environmental analysis

In this section, primary energy consumption and CO<sub>2</sub> emissions of the system under study will be evaluated. To that aim, its performance will be compared to five alternatives which are commonly used for DHW production. Thus, the comparison considers a total of six systems:

- **HP + PV.** This is the system under analysis which has been described in Section 2. It consists of a 1.5 kW<sub>TH</sub> compact heat pump which heats water within its 190 litre water tank (Table 1(a)). The heat pump is powered by two 235 W<sub>p</sub> photovoltaic panels (Table 1(b)) and the grid. Besides, if the heat pump is OFF, the PV production is used to power an electric resistance within the tank.
- **HP.** It consists of the same heat pump which is powered only by the grid (the electric heater is not used).
- **Boiler.** A natural gas boiler with a seasonal efficiency of 92%. This system will be considered the reference one for comparison purposes.
- **Boiler + ST.** A natural gas boiler with a seasonal efficiency of 92% and solar thermal panels with a solar contribution of 60% of the thermal demand.
- **Heater.** An 80 litre water tank with a 1.5 kW electric resistance.
- **Heater + PV.** An 80 litre water tank with a 1.5 kW electric resistance powered by 4 PV panels (a total of 940 W<sub>p</sub>).

Sketches of the three systems under comparison, which use solar energy, are depicted in Figure 5.

The HP+PV system has been experimentally studied during one year. The DHW demand results in an energy demand of 2247.6 kWh<sub>TH</sub> throughout the year according to the measurements. Besides, the 190 litre water tank losses have been experimentally estimated at 596.7 kWh<sub>TH</sub>, resulting in a total thermal demand of 2844.3 kWh<sub>TH</sub>. In order to cover such a demand, the

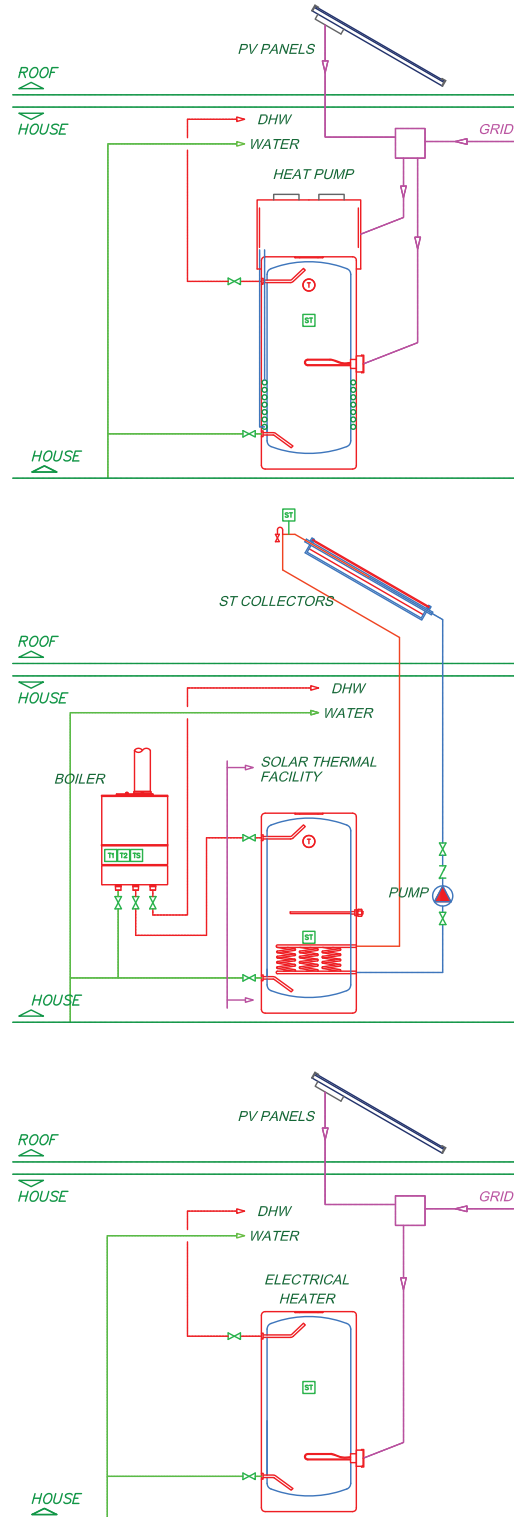


Figure 5: Sketch of the facilities of the comparison which use solar energy. Top: HP + PV. Middle: Boiler + ST. Bottom: Heater + PV



Table 2: Annual energy consumption and CO<sub>2</sub> emissions for the systems under consideration.

	Units	HP + PV	HP	BOILER	BOILER + ST	HEATER	HEATER + PV
DHW demand	kWh	2,247.6	2,247.6	2,247.6	2,247.6	2,247.6	2,247.6
Water tank heat loss	kWh	596.7	596.7	0.0	0.0	358.0	358.0
Total demand	kWh	2,844.3	2,844.3	2,247.6	2,247.6	2,605.6	2,605.6
Grid electricity consumption	kWh	317.6	831.7	45.0	72.7	2,605.6	1,038.6
Natural Gas consumption	kWh	0.0	0.0	2,443.0	977.2	0.0	0.0
Non-renewable primary energy	kWh	635.2	1,663.3	3,021.6	1,318.1	5,211.2	2,077.2
Non-renewable primary energy (*)	kWh/m <sup>2</sup>	7.1	18.5	33.6	14.6	57.9	23.1
FSAV nRPE	-	79.0%	45.0%	0.0%	56.4%	-72.5%	31.3%
Ratio nRPE	-	4.76	1.82	1.00	2.29	0.58	1.45
CO <sub>2</sub> emissions	kg CO <sub>2</sub>	113.4	296.9	631.7	272.2	930.2	370.8
CO <sub>2</sub> emissions (*)	kg CO <sub>2</sub> /m <sup>2</sup>	1.3	3.3	7.0	3.0	10.3	4.1
FSAV CO <sub>2</sub> emissions	-	82.1%	53.0%	0%	56.9%	-47.3%	41.3%
Ratio CO <sub>2</sub> emissions	-	5.57	2.13	1.00	2.32	0.68	1.70

(\*) For a dwelling surface of 90 m<sup>2</sup>

433 *HP+PV* system has been found to consume 317.6 kWh  
434 of electricity from the grid, while the rest (514.1 kWh)  
435 has been provided by the PV panels.

436 The *SPF* of the *HP+PV* system is defined as the frac-  
437 tion between its thermal heat production over its elec-  
438 tricity consumption from the grid in real working con-  
439 ditions throughout a year:

$$SPF_{HP+PV} = \frac{Q_{TOT}}{E_{GD}} \quad (7)$$

440 The total thermal, electrical and/or natural gas de-  
441 mand of the other systems have been estimated from  
442 the data obtained for the *HP+PV* system. The results  
443 are summarized in Table 2.

444 The *HP* system would have the same total thermal de-  
445 mand as the *HP+PV* one. Its seasonal performance fac-  
446 tor is considered to be  $SPF_{HP} = 3.42$  (obtained from  
447 the experimental measurements), resulting in an elec-  
448 tricity consumption from the grid of 831.7 kWh.

449 In the case of the *Boiler*, as there are no water  
450 tank losses, the total demand (2247.6 kWh<sub>TH</sub>) is lower  
451 than in the previous cases. The seasonal efficiency  
452 of the boiler (*Boiler* has been estimated at 92% and  
453 its electrical consumption at 2% of the total demand.  
454 Consequently, the natural gas consumption results in  
455 2443 kWh.

456 For the *Boiler + ST* system, the same considerations  
457 as in previous system have been made regarding: the to-  
458 tal demand, the boiler efficiency and its electrical con-  
459 sumption. The solar thermal facility has been calculated  
460 by using the f-chart method to cover 60% of the total  
461 demand, resulting in a system with a 120 litres water  
462 tank and a 2.2 m<sup>2</sup> thermal solar panel. Besides, a 30 W  
463 circulation pump has been estimated to work 5 hours  
464 a day. The results show a natural gas consumption of  
465 977.2 kWh and an electricity consumption of 72.7 kWh.

Table 3: System efficiencies and energy conversion factors for Spain (IDAE, 2016).

	value	units
$SPF_{HP+PV}$	8.96	
$SPF_{HP}$	3.42	
$\tilde{\eta}_{Boiler}$	0.92	
$PEF_{EL}$	2.0	kWh <sub>nRPE</sub> /kWh
$PEF_{NG}$	1.2	kWh <sub>nRPE</sub> /kWh
Electricity emissions	0.357	gCO <sub>2</sub> /kWh
Natural Gas emissions	0.252	gCO <sub>2</sub> /kWh

In the case of the electrical heater (*Heater* system), the water tank losses have been calculated by means of the AISLAM software (IDAE, 2007), resulting in a 60% of the ones of the *HP+PV* system, due to its smaller size. The result is a total demand of 2605.6 kWh<sub>TH</sub> which requires the same amount of electricity (100% efficiency).

If the *Heater + PV* system is considered, the water tank losses would be the same as with the *Heater* system. Although the electricity consumption of the heater is the same in both cases (2605.6 kWh), only 1038.6 kWh is consumed from the grid, as the difference is provided by the PV panels. The contribution of each PV panel has been obtained from the experimental measurements of electricity production per panel within the *HP+PV* system.

From the final energy consumption, the non-renewable primary energy consumption and CO<sub>2</sub> emissions have been obtained by applying the conversion factors in Table 3. In order to obtain the non-renewable primary energy consumption and CO<sub>2</sub> emissions by square metre, a surface of 90 m<sup>2</sup> has been estimated for

488 a 4 member family dwelling.

489 If the *Boiler* system is taken as the reference system,  
 490 the following ratios may be defined. On the one hand,  
 491 the *savings fraction* of non-renewable primary energy,  
 492 indicates the percentage of non-renewable primary en-  
 493 ergy consumption which is saved by the system under  
 494 consideration.

$$FSAV_{nRPE} (\%) = \frac{nRPE_{ref} - nRPE_{sys}}{nRPE_{ref}} \quad (8)$$

495 On the other hand, the Primary Energy Ratio  
 496 ( $PER_{nRE}$ ) indicates the relation between the non-  
 497 renewable primary energy employed by the reference  
 498 and by the analysed system for the same energy de-  
 499 mand.

$$PER_{nRE} = \frac{nRPE_{ref}}{nRPE_{sys}} \quad (9)$$

500 Equivalently, similar savings factor and ratio can be  
 501 defined for CO<sub>2</sub> emissions between the system under  
 502 consideration (*sys*) and the reference system (*ref*).

$$FSAV_{CO_2} (\%) = \frac{CO_{2,ref} - CO_{2,sys}}{CO_{2,ref}} \quad (10)$$

$$PER_{CO_2} = \frac{CO_{2,ref}}{CO_{2,sys}} \quad (11)$$

503 As can be observed in Table 2, the lowest CO<sub>2</sub> emis-  
 504 sions and non-renewable primary energy consumption  
 505 correspond to the *HP+PV* system. With this system,  
 506 the annual primary energy savings in comparison with  
 507 the reference is  $FSAV_{nRPE} = 79\%$ , which means it is  
 508 4.76 times more efficient in the use of primary energy  
 509 than the reference system. Furthermore, the annual CO<sub>2</sub>  
 510 emissions savings factor is even higher,  $FSAV_{CO_2} =$   
 511  $82.1\%$ , being 5.57 times more efficient than the refer-  
 512 ence system regarding emissions.

513 The heater presents the worst annual performance  
 514 of all the systems, consuming more primary energy  
 515 ( $FSAV_{nRPE} = -72.5\%$ ) and emitting more carbon diox-  
 516 ide ( $FSAV_{CO_2} = -47.3\%$ ) than the reference, which is  
 517 the second worst system in both parameters. The rest of  
 518 the systems perform better than the reference, being the  
 519 boiler with solar thermal panels the best option among  
 520 them ( $FSAV_{nRPE} = 56.4\%$   $FSAV_{CO_2} = 56.9\%$ ).

521 Quite significant for a system is the non-renewable  
 522 primary energy consumption per dwelling surface area  
 523 (Figure 6). This value is usually limited within the  
 524 E.U. countries, so that high primary energy consump-  
 525 tions are not allowed. The sum of non-renewable  
 526 primary energy consumption for the services of air  
 527 conditioning, heating and DHW is typically limited

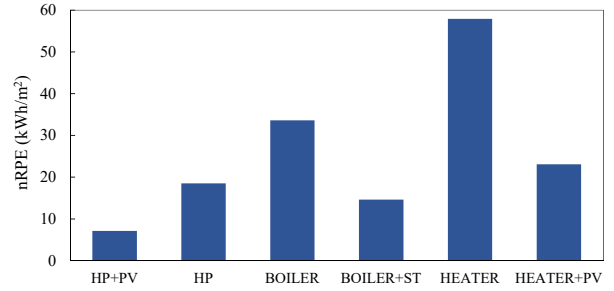


Figure 6: Annual non-renewable primary energy consumption for a 90 m<sup>2</sup> dwelling.

528 to values up to 15 to 40 kWh<sub>nRPE</sub>/m<sup>2</sup> (E.U. Recom-  
 529 mendation of 29 July 2016). This means that using  
 530 an electric heater (57.9 kWh<sub>nRPE</sub>/m<sup>2</sup>) or a boiler  
 531 (33.6 kWh<sub>nRPE</sub>/m<sup>2</sup>) for DHW production is not an op-  
 532 tion. In this way, the real consumption of a heater  
 533 with PV panels (23.1 kWh<sub>nRPE</sub>/m<sup>2</sup>), a heat pump  
 534 (18.5 kWh<sub>nRPE</sub>/m<sup>2</sup>) or a boiler with solar thermal pan-  
 535 els (14.6 kWh<sub>nRPE</sub>/m<sup>2</sup>) may be valid options depend-  
 536 ing on the applicable limitation, being the boiler with so-  
 537 lar thermal panels the solution with the lowest primary  
 538 energy consumption among them. Once again, the sys-  
 539 tem under study (*HP+PV*) beats the other systems of the  
 540 comparison by far, consuming only 7.1 kWh<sub>nRPE</sub>/m<sup>2</sup>.

### 3.4. Economic analysis

This study is aimed at analysing the economic via-  
 bility of the heat pump water heater powered by photo-  
 voltaic panels and the grid (*HP+PV*) in comparison with  
 conventional DHW systems. The same systems as in the  
 previous section have been chosen for the comparison.

The economic analysis, whose results are shown in  
 Table 4, takes into account the annual costs for invest-  
 ment, maintenance, residual value, replacement and en-  
 ergy cost during the system lifetime. The annualized  
 cost for a system is calculated by means of the annuity  
 method.

The lifetime of each system component is estimated  
 to be: PV panels: 25 years; Inverter and inhibitor: 12.5  
 years; Solar thermal collectors and tank: 20 years; Heat  
 pump, boiler and electrical heater: 18 years (accord-  
 ing to the ranges proposed on Annex D of EN 15459-  
 1:2018). The initial cost and the annual maintenance  
 cost are determined from real prices provided by three  
 companies that use to work at local level. The provided  
 costs were finally discussed and agreed with the three  
 companies to be a good approach to the real prices of-  
 fered at present in Spain.

The maintenance cost for the PV panels has been  
 quantified as 30 €/year for two panels and 40 €/year

Table 4: Techno-economic study results for a 25 year lifetime (Energy cost 0.15 €/kWh).

	HP + PV	HP	BOILER	BOILER + ST	HEATER	HEATER + PV
<b>INVESTMENT</b>	€	€	€	€	€	€
PV panels	400.0	0.0	0.0	0.0	0.0	800.0
Inverter + Inhibitor	300.0	0.0	0.0	0.0	0.0	600.0
Solar thermal collectors	0.0	0.0	0.0	1,300.0	0.0	0.0
Heat Pump	1,200.0	1,200.0	0.0	0.0	0.0	0.0
Boiler	0.0	0.0	1,200.0	1,200.0	0.0	0.0
Electric heater	0.0	0.0	0.0	0.0	500.0	500.0
<b>TOTAL INVESTMENT MATERIAL</b>	<b>1,900.0</b>	<b>1,200.0</b>	<b>1,200.0</b>	<b>2,500.0</b>	<b>500.0</b>	<b>1,900.0</b>
Design, planning and commissioning	200.0	200.0	60.0	120.0	50.0	200.0
General costs associated to works	380.0	240.0	240.0	500.0	100.0	380.0
Indirect costs and industrial benefits	95.0	60.0	60.0	125.0	25.0	95.0
<b>TOTAL INVESTMENT COST</b>	<b>2,575.0</b>	<b>1,700.0</b>	<b>1,560.0</b>	<b>3,245.0</b>	<b>675.0</b>	<b>2,575.0</b>
<b>REPLACEMENT COST</b>	€/year	€/year	€/year	€/year	€/year	€/year
PV panels (NL=25 years)	0.00	0.00	0.00	0.00	0.00	0.00
Inverter + Inhibitor (NL=12,5 years)	11.65	0.00	0.00	0.00	0.00	23.30
Solar thermal collectors (20 years)	0.00	0.00	0.00	12.62	0.00	0.00
Heat Pump (18 years)	18.12	18.12	0.00	0.00	0.00	0.00
Boiler (18 years)	0.00	0.00	18.12	18.12	0.00	0.00
Electric heater (18 years)	0.00	0.00	0.00	0.00	7.55	7.55
<b>TOTAL REPLACEMENT COST</b>	<b>29.77</b>	<b>18.12</b>	<b>18.12</b>	<b>30.74</b>	<b>7.55</b>	<b>30.85</b>
<b>MAINTENANCE COST</b>	€/year	€/year	€/year	€/year	€/year	€/year
PV panels + Inverter + Inhibitor	30.00	0.00	0.00	0.00	0.00	40.00
Solar thermal collectors	0.00	0.00	0.00	60.00	0.00	0.00
Heat pump	60.00	60.00	0.00	0.00	0.00	0.00
Boiler	0.00	0.00	60.00	60.00	0.00	0.00
Electric heater	0.00	0.00	0.00	0.00	20.00	20.00
<b>TOTAL MAINTENANCE COST</b>	<b>90.00</b>	<b>60.00</b>	<b>60.00</b>	<b>120.00</b>	<b>20.00</b>	<b>60.00</b>
<b>OPERATION-ENERGY</b>	€/year	€/year	€/year	€/year	€/year	€/year
Energy Cost (Electricity or Gas)	63.52	166.33	155.56	73.17	521.12	207.72
Power Cost (Electricity or Gas)	40.00	40.00	60.00	60.00	80.00	80.00
<b>TOTAL ENERGY COST</b>	<b>103.52</b>	<b>206.33</b>	<b>215.56</b>	<b>133.17</b>	<b>601.12</b>	<b>287.72</b>
<b>ANNUALIZED COSTS</b>	€/year	€/year	€/year	€/year	€/year	€/year
Investment	118.95	78.53	72.06	149.90	31.18	118.95
Replacement	29.77	18.12	18.12	30.74	7.55	30.85
Maintenance	87.38	58.25	58.25	116.50	19.42	58.25
Energy (Electricity or Gas)	100.50	200.32	209.28	129.29	583.62	279.34
<b>TOTAL ANNUALIZED COST</b>	<b>336.61</b>	<b>355.23</b>	<b>357.72</b>	<b>426.45</b>	<b>641.77</b>	<b>487.40</b>

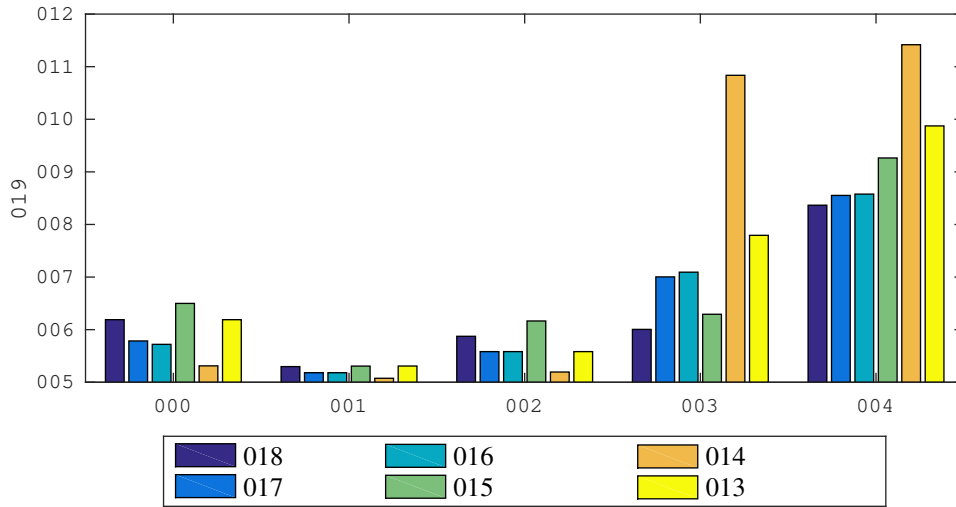


Figure 7: Individual annual cost contributions and total cost of the systems.

566 for four panels. This same cost has been quantified at 597  
 567 60 €/year for the solar thermal collectors. For the heat 598  
 568 pump and the boiler, a maintenance cost of 60 €/year 599  
 569 is considered, while 20 €/year is used for the electric 600  
 570 heater. 601

571 The period under consideration for the study is 25 602  
 572 years. An inflation rate of 3% and a market discount 603  
 573 rate of 3% have also been considered. Besides, the 604  
 574 units are paid with a 5 year credit at an interest rate 605  
 575 of 5%. On the one hand, the energy cost of electric- 606  
 576 ity is considered to be 0.20 €/kWh and its power cost 607  
 577 40 €/year for the heat pump systems (*HP* and *HP+PV*) 608  
 578 and 80 €/year for the systems with electrical heaters. 609  
 579 On the other hand, the energy and power cost of natural 610  
 580 gas are 0.06 €/kWh and 60 €/year, respectively, for the 611  
 581 systems using boilers. The prices are based on official 612  
 582 published data (CNMC, 2019; CNMC, 2018). 613

583 If focusing on the investment cost, the results in Ta- 614  
 584 ble 4 show that the cheapest alternative for DHW pro- 615  
 585 duction is, by far, the electric heater. Buying a heat 616  
 586 pump and two photovoltaic panels for the same use 617  
 587 would be almost 4 times more expensive. This may 618  
 588 trick consumers into making this choice, however, when 619  
 589 all lifetime costs are considered, the electric heater be- 620  
 590 comes the worst choice and the heat pump with PV pan- 621  
 591 els the best one. The main reason is that the electric 622  
 592 heater is much less efficient than a heat pump, leading 623  
 593 to higher energy consumption. Furthermore, the dif- 624  
 594 ference in price between the natural gas and electricity, 625  
 595 results in lower total annualized costs for the solutions 626  
 596 with boilers than for those with electric heaters. 627

Figure 7 is the comparison of the individual annual cost contributions and the total cost between the systems.

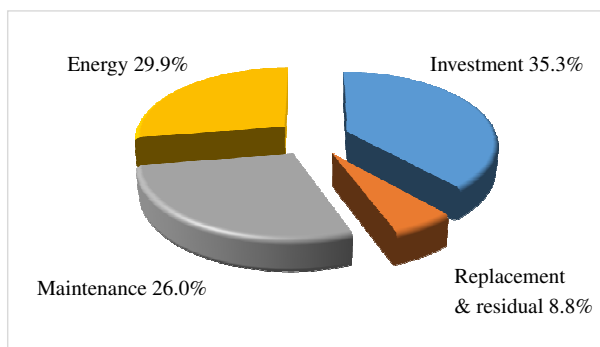
As it can be appreciated, the energy cost for the electric (*Heater*) is huge in comparison with the investment cost, 583.6 €/year vs 31.2 €/year, resulting in a total annualized cost of 641.8 €/year.

If the heater is powered partly by photovoltaic panels (*Heater + PV*), the cost of energy drops to 279.3 €/year and the investment cost rises to 119 €/year, resulting in a cheaper choice (487.46 €/year) than the heater alone.

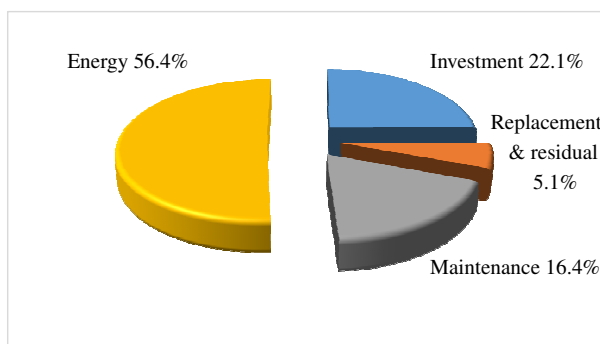
The use of a simple boiler requires an investment of 72.1 €/year, being the total annualized cost of 357.7 €/year significantly lower than for the *Heater* and the *Heater + PV*, mainly due to the lower energy costs of natural gas. Its energy cost is 209.3 €/year, the maintenance cost is 58.3 €/year and the replacement and residual cost is 18.1 €/year.

If the *boiler* is combined with solar thermal collectors, the energy expenditure drops significantly to 129.3 €/year, however, it does not compensate for the rise in investment (149.9 €/year), maintenance (116.5 €/year) and replacement and residual cost (30.7 €/year). The result is that using solar thermal collectors makes the total annualized cost higher (426.4 €/year).

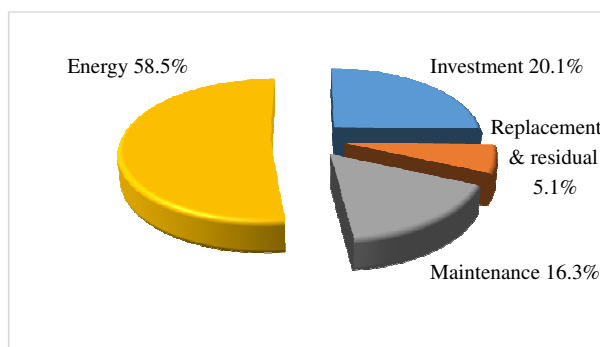
The solution with a heat pump (*HP*), if compared with the boiler, implies similar energy (200.3 €/year), investment (78.5 €/year), maintenance and replacement costs, resulting in a slightly lower total annualized cost (355 €/year).



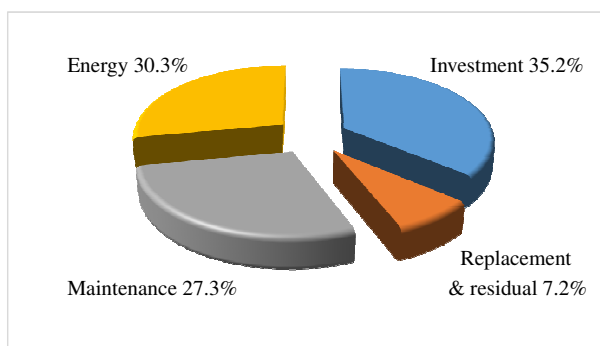
(a) HP + PV. Total Cost of 337 €/year.



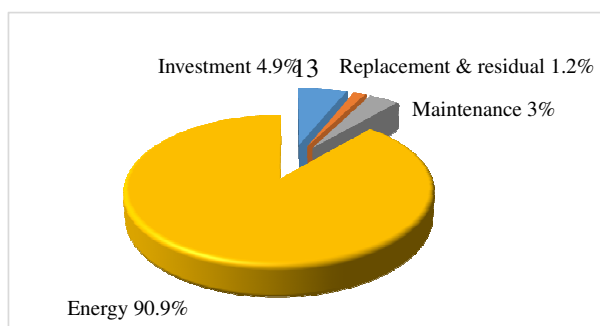
(b) HP. Total Cost of 355 €/year.



(c) Boiler. Total Cost of 358 €/year.



(d) Boiler + ST. Total Cost of 426 €/year.



If the heat pump is combined with photovoltaic panels ( $HP + PV$ ), the required investment obviously increases (119 €/year), but the energy requirements are significantly reduced to 100.5 €/year, resulting in similar total annualized cost of 336.6 €/year, which is also the lowest one of the comparison.

Figure 8, shows the individual weight of each annualized cost in the total cost for the different systems. For example, in the figure, the most significant cost of each system can be appreciated. For the *heater*, the energy cost represents 90.9% and investment is only 4.9%. The energy cost is also significant for the *Boiler* (58.5%), the *heater + PV* (57.3%) and the *HP* (56.4%), but not that important for the *boiler + ST* (30.3%) or the *HP + PV* (29.9%). For the latter options, the investment and maintenance costs are even more important than the energy cost ( $HP+PV$ , maintenance of 26% and investment of 35.3%, *boiler+ST* maintenance of 27.3% and investment of 35.2%).

From the results, it can then be concluded, that the heat pump with the photovoltaic panels is the cheapest option, although similar to using only a heat pump or only a boiler. However, the results of the economic study depend highly on the energy prices, which can vary in time and from one country to another. Therefore, the same comparison has been carried out for different electricity prices, ranging from 0.1 €/kWh to 0.4 €/kWh.

As can be observed in Figure 9, if the electricity price is very low (0.1-0.15 €/kWh), the heat pump (without PV panels) would be the economically most interesting choice. If the electricity price is higher, the heat pump with PV becomes more interesting in comparison with the heat pump (without PV panels). It can be also seen that the impact of the energy price on the total annualized cost of the  $HP+PV$  system is low. This reduces the uncertainty of this long term economic analysis.

### 3.5. Results extrapolation tools

In this section, the necessary tools are provided for the extrapolation of the results of this work to other locations with similar climate conditions (Mediterranean climate). To that aim, the experimental results have been used to obtain the correlations of Fig. 10 and Fig. 11.

On the one hand, in Fig. 10 there is a representation of the solar contribution (Eq. 6) versus daily solar irradiation for all daily measurements. It shows that solar contributions of up to more than 80% may be reached on days with high irradiation.

On the other hand, Figure 11 shows the relation between the daily average seasonal performance factor of

the heat pump  $SPF_{HP}$  versus the average ambient temperature during its working hours (from 10:00 to 14:00 solar time). It shows a significantly better performance of the heat pump for high ambient temperatures than for low ones.

From equations 1 to 6, Eq. 12 is deduced, which allows us to obtain the photovoltaic electrical energy consumption of the heat pump.

$$E_{PV,HP} = \frac{Q_{TOT} \cdot SC - E_{PV}}{SPF_{HP}} \quad (12)$$

Finally, in order to determine the grid electricity consumption of the heat pump, Eq. 13 may be used (from equations 2 and 5).

$$E_{GD} = \frac{Q_{HP}}{SPF_{HP}} - E_{PV,HP} \quad (13)$$

Consequently, once the climate conditions at a different location are known, the energetic needs of the  $HP+PV$  system can be determined as well as its operating cost. Thus, the results of this study can be extrapolated to other locations with similar climate conditions (Mediterranean climate) and domestic hot water demand.

## 4. Conclusions

This work has analysed the use of a heat pump powered by photovoltaics and the grid for domestic hot water production purposes. The  $HP+PV$  system does not feed electricity to the electrical grid and does not use batteries.

The economic study has shown that the  $HP+PV$  solution is competitive for domestic hot water production. In addition, the combination of heat pumps and photovoltaics should be considered as a decarbonized solution for nearly zero energy buildings, since it has a minimal non-renewable primary energy consumption.

The total annualized cost of the proposed solution (337 €/year) is considerably lower than other options in the market and similar to using only a heat pump or a boiler. The environmental study attests that the system under study outperforms by far any other solution: savings in primary energy of  $FSAV_{nrPE} = 79\%$  and in  $CO_2$  emissions  $FSAV_{CO_2} = 82\%$  vs. a boiler. The boundary of the techno-economic analysis is the system itself.

The low electricity consumption from the grid of the  $HP+PV$  system, yields to a low dependence of the total annualized cost on the electricity price. This reduces the uncertainty of a long term economic analysis.

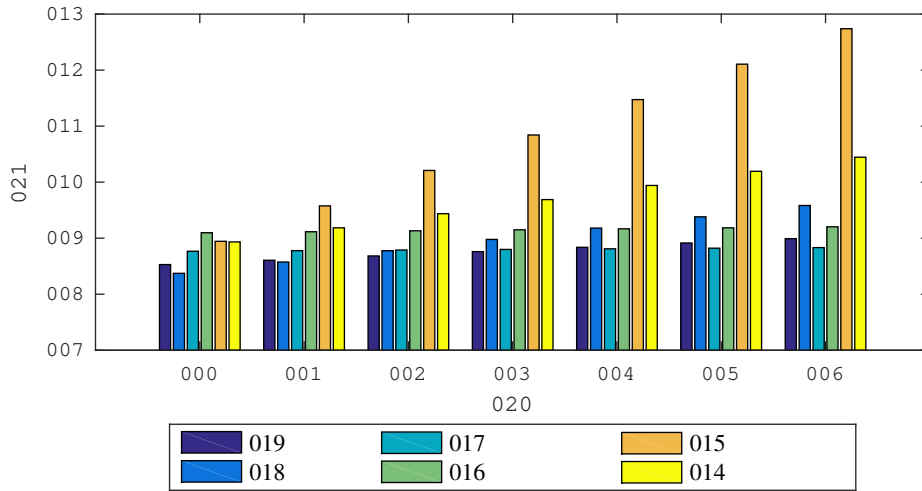


Figure 9: Influence of the electricity price on the total annualized cost.

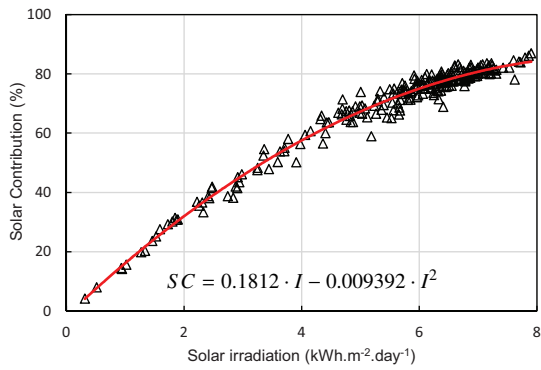


Figure 10: Solar contribution to the heat pump consumption (*HP+PV system*) as a function of the irradiation on the surface of the PV panels (45°). Correlation in red.

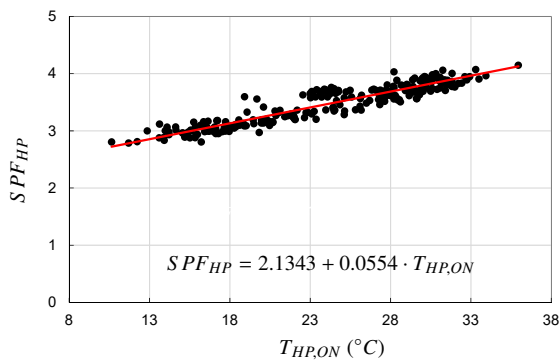


Figure 11: Seasonal performance factor of the heat pump for one day versus the average ambient temperature during its working time.

721 The interaction with the electrical grid plays an im-  
 722 portant role when a heat pump is supported by photo-  
 723 voltaics. The system has been shown to be friendly to-  
 724 wards the electrical network:

- 725 • PV production is 100% self-consumed by the sys-  
 726 tem.
- 727 • The system does not feed electricity to the grid.
- 728 • Very low electrical consumption peaks.

729 This work has provided valuable experimental data  
 730 for the design and comprehension of the operation of  
 731 facilities implementing the system under study.

732 Finally, experimental correlations for the solar contri-  
 733 bution and the seasonal performance factor of the heat  
 734 pump have been obtained. They can be used to extrapo-  
 735 late the results of this work to other locations with sim-  
 736 ilar climatic conditions.

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